SECTION-B

Amplitude Modulation (AM):

- AM Generation (Modulation)
- AM Demodulation
- Generation of DSBSC wave
- Detection of DSBSC wave
- Generation of SSB wave
- Detection of SSB wave
- VSB Modulation

Amplitude Modulation

The Complex Envelope of an AM signal is given by

 $g(t) = A_c[1+m(t)]$

 A_c indicates the power level of AM and m(t) is the Modulating Signal

Representation of an AM signal is given by

 $s(t) = A_c[1 + m(t)]\cos\omega_c t$

> $A_c[1+m(t)]$ In-phase component x(t)

▶ If m(t) has a peak positive values of +1 and a peak negative value of -1 AM signal → 100% modulated

Envelope detection can be used if % modulation is less than 100%.

AM Signal Waveform



AM Spectrum



Amplitude Modulation



Low-level generation

- In modern radio systems, modulated signals are generated via digital signal processing (DSP).
- With DSP many types of AM modulation are possible with software control

(including DSB with carrier, SSB suppressed-carrier and independent sideband, or ISB).

Collector Modulation



High-level generation

- High-power AM transmitters (such as those used for AM broadcasting) are based on highefficiency class-D and class-E power amplifier stages, modulated by varying the supply voltage.
- Older designs (for broadcast) also generate AM by controlling the gain of the transmitter's final amplifier (generally class-C, for efficiency). The following types are for vacuum tube transmitters (but similar options are available with transistors):

AM Demodulation

- Square law Detector
- Linear Diode (Envelope) Detector



- Linear detector utilizes the rectification characteristic of a diode.
- The modulated carrier voltage is applied to the series combination of diode and the load impedance consisting of resistor R in shunt with capacitor C.
- Since applied voltage is of large magnitude, the operation takes place essentially over the linear region of the dynamic current-voltage characteristic of the diode.
- The idealized linear dynamic current-voltage characteristic of the diode detector. Assuming capacitor C to be absent, the total impedance in series circuit is (ra + R) where ra is the dynamic anode resistance of the diode.

 O/P voltage curve is of spiky nature but it almost traces the envelope of the modulated carrier voltage and hence it is nothing but the original modulation voltage

 The departure of this output voltage from the envelope may be reduced by proper choice of R and C depending upon the modulation frequency and depth of modulation

Double Side Band Suppressed Carrier (DSBSC)

Power in a AM signal is given by

$$s^{2}(t) = \frac{1}{2}A_{c}^{2} + \frac{1}{2}A_{c}^{2}\langle m^{2}(t) \rangle$$

Carrier Power



DSBSC is obtained by eliminating carrier component If *m(t)* is assumed to have a zero DC level, then

$$s(t) = A_c m(t) \cos \omega_c t$$

Spectrum
$$\Rightarrow$$
 $S(f) = \frac{A_c}{2} \left[M \left(f - f_c \right) + M \left(f + f_c \right) \right]$
Power $\Rightarrow \left\langle s^2(t) \right\rangle = \frac{1}{2} A_2 \left\langle m_2(t) \right\rangle$

Modulation Efficiency ->

$$E = \frac{\left\langle m^{2}(t) \right\rangle}{\left\langle m^{2}(t) \right\rangle} \times 100 = 100\%$$

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Disadvantages of DSBSC:

• Less information about the carrier will be delivered to the receiver.

DSBSC Modulation



DSBSC Generation using Balanced Modulator



DSBSC Generation using Ring Modulator





DSBSC Demodulation

- Synchronous Detection
- Envelope Detection after suitable carrier reinsertion

Carrier Recovery for DSBSC Demodulation

> Coherent reference for product detection of DSBSC can not be obtained by the use of ordinary PLL because there are no spectral line components at f_c .



⁽a) Costas Phase-Locked Loop

Single Sideband (SSB) Modulation

 $|f| < f_c$

 $|f| > f_c$

- An upper single sideband (USSB) signal has a zero-valued spectrum for
 - A lower single sideband (LSSB) signal has a zero-valued spectrum for
- SSB-AM popular method ~ BW is same as that of the modulating signal. Note: Normally SSB refers to SSB-AM type of signal



Single Sideband Signal

Theorem : A SSB signal has Complex Envelope and bandpass form as:

$$g(t) = A_c \left[m(t) \pm j \hat{m}(t) \right]$$

$$s(t) = A_c[m(t) \cos \omega_c t + \hat{m}(t) \sin \omega_c t] \qquad \text{Upper sign (-)} \rightarrow \text{USSB}$$

Lower sign (+) $\rightarrow \text{LSSB}$

 $\hat{m(t)}$ – Hilbert transform of $m(t) \rightarrow \hat{m(t)} \equiv m(t) * h(t)$ Where $h(t) = \frac{1}{\pi t}$

$$H(f) = \Im[h(t)] \quad \text{and} \quad H(f) = \begin{cases} -j, & f > 0\\ j, & f < 0 \end{cases}$$

Hilbert Transform corresponds to a -90° phase shift

Single Sideband Signal

Proof: Fourier transform of the complex envelope

 $G(f) = A_c \left\{ M(f) \pm f \mathbb{E}[m(t)] \right\} = A_c \left\{ M(f) \pm j M(f) \right\} \qquad \text{Upper sign } \Rightarrow \text{USSB} \\ \text{Lower sign } \Rightarrow \text{LSSB} \\ \text{Using} \qquad m(t) \equiv m(t) * h(t) \qquad \Rightarrow G(f) = A_c M(f) [1 \pm j H(f)] \\ G(f) = \begin{cases} 2A_c M(f), & f > 0 \\ 0, & f < 0 \end{cases} \\ \text{Recall} \qquad V(f) = \frac{1}{2} \left\{ G(f-f) + G * [-(f+f)] \right\} \end{cases}$

$$S(f) = A_c \begin{cases} M(f-f_c), f > f_c \\ 0, f < f_c \end{cases} + A_c \begin{cases} 0, f > -f_c \\ M(f+f_c), f < -f_c \end{cases}$$



If lower signs were used \rightarrow LSSB signal would have been obtained

Weaver's Method for Generating SSB.



Generation of VSB



(e) VSB Filter Constraint